

### THREE-PHASE AC CHOPPER WITH IGBT'S

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**Abstract.** This paper describes two circuits three-phase ac chopper realised with IGBT's with high carrier wave frequency (chopper frequency). The first circuit described in this article is a three-phase chopper functioning with inductive load. In both situations the power sources are symmetrically three-phases. Also, the simulation waveforms of the load and input currents for the power circuits are presented.

#### Introduction

A.C. Choppers have been widely used to control average load power from a fixed ac source. The common applications are industrial heating, light dimming, and ac motor speed control. The advantages of the ac choppers are simplicity, ability of controlling large amount of power, and high efficiency.

The IGBT's controls for both circuits are made using uniform technique PWM, presented in detail in (e.g. [5]), where the control signal  $V_{com1}$  is obtained by comparing a triangular wave with a reference voltage used for modifying the duty factor  $D$  and, implicitly, the load voltage. The control voltages  $V_{com1}$  and  $V_{com2}$  are opposite signals. In order to obtain identical voltages on the three-phase system, the index of modulation  $m$  must be multiple of six. The chopper frequency was chosen to be  $f_s = 6\text{kHz}$ . The power circuits with filters are used to obtain the sinewave of the input current.

#### Power circuit

Figure 1 shows the power circuit of the three-phase ac chopper in the case of resistive load. The circuit contains one ac switch  $Q$  with IGBT and six diodes. The IGBT control strategy is presented in Figure 2. Suppose the ac-input voltage is expressed as:

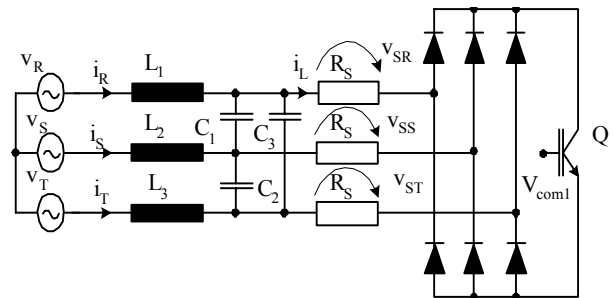


Figure 1. Power circuit of three-phase ac chopper for resistive loads.

$$\begin{aligned}
 v_R &= V\sqrt{2} \cos \omega t \\
 i_R &= I\sqrt{2} \cos(\omega t - \varphi), \quad \omega = \frac{2\pi}{T} \\
 v_S &= V\sqrt{2} \cos\left(\omega t - \frac{2\pi}{3}\right) \\
 i_R &= I\sqrt{2} \cos\left(\omega t - \frac{2\pi}{3} - \varphi\right) \\
 v_T &= V\sqrt{2} \cos\left(\omega t - \frac{4\pi}{3}\right) \\
 i_T &= I\sqrt{2} \cos\left(\omega t - \frac{4\pi}{3} - \varphi\right)
 \end{aligned} \tag{1}$$

$\varphi$  - represent the shift angle between the voltage and the current of the power sources.

For a symmetrical three-phase system, we have

$$v_R + v_S + v_T = 0 ; i_R + i_S + i_T = 0 \tag{2}$$

The index of modulation is:

$$m = \frac{f_s}{f} = 6l, \quad l \in \mathbb{N} \tag{3}$$

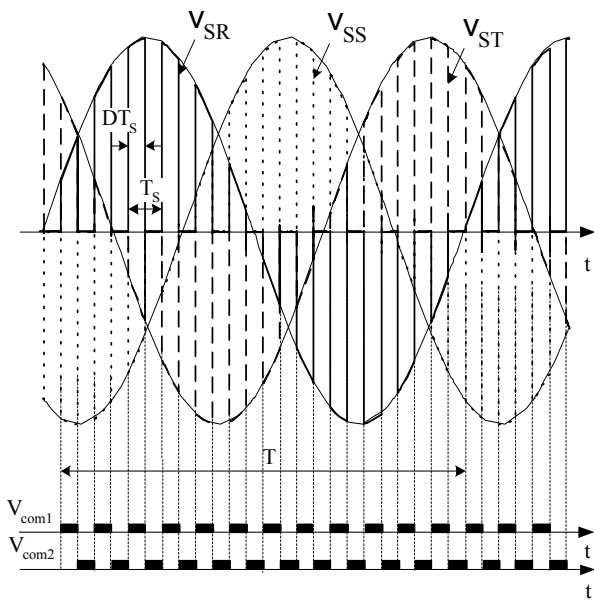


Figure 2 The waveforms of the load voltage and the control signal  $V_{com1}$

Considering the condition (3) the waveforms of the load voltage are presented in Figure 2.

The most cases in practice the load has an inductive character. In this case, for a three-phase system, the load can be connected in the shape of triangle or of a star. Figure 3 presents the circuit of a three-phase ac chopper in which the load is connected in the shape of a star without a ground wire

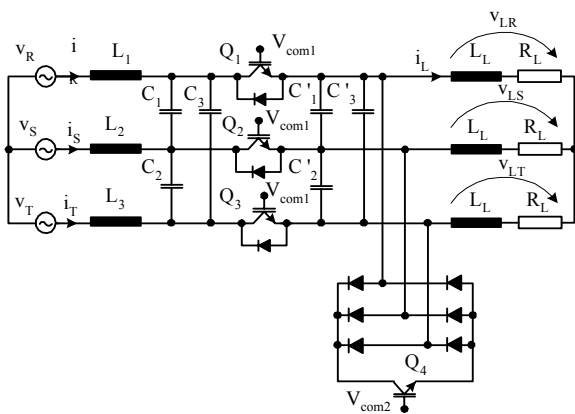


Figure 3. Three-phase ac chopper for an inductive load connected in the shape of a star without ground wire

The chopper in Figure 3 is realised by using nine switching diodes and four IGBT's. The three  $Q_1$ ,  $Q_2$ , and  $Q_3$  IGBT's directly connected to the three-phase system are controlled simultaneously with the control signal  $V_{com1}$  and the  $Q_4$  IGBT with the control signal  $V_{com2}$ . The

IGBT's  $Q_1$ ,  $Q_2$ ,  $Q_3$  regulates the power delivered

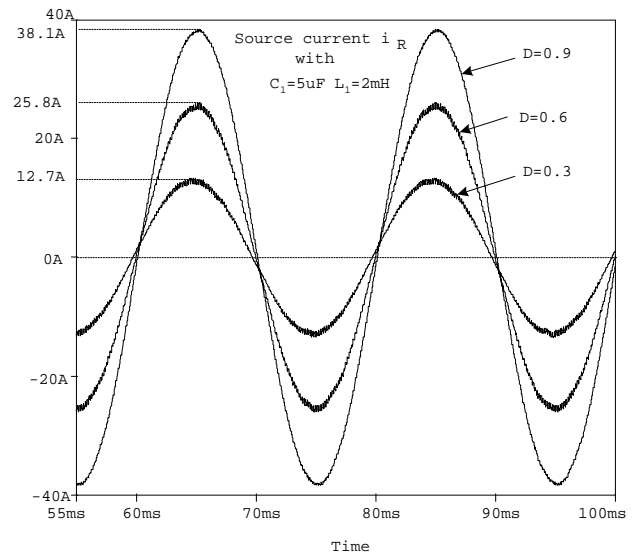


Figure 4. Source current  $i_R$  waveforms.

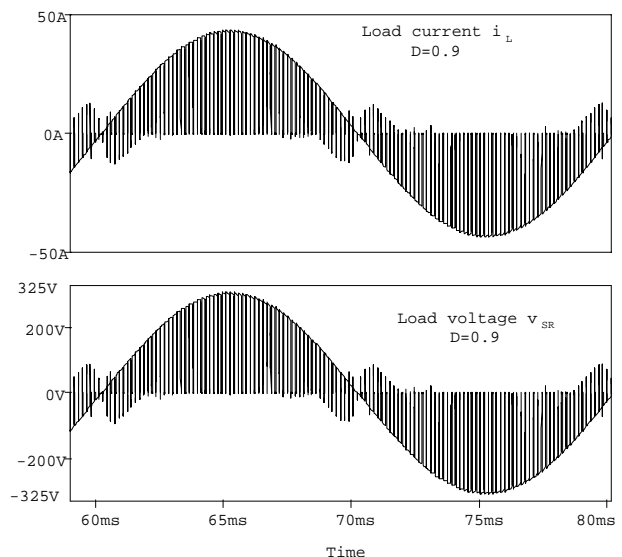


Figure 5. Load current  $i_L$  and load voltage  $v_{SR}$

to the load, IGBT  $Q_4$  provides the freewheeling path to discharge the stored energy when the series switch is turned off. The capacities  $C'_1$ ,  $C'_2$  and  $C'_3$  are meant to ensure the freewheeling path to the load currents starting with the moment when the IGBT's  $Q_1$ ,  $Q_2$ ,  $Q_3$ , are off and the IGBT  $Q_4$  is on. For the two circuits presented in Figure 1 and Figure 3, the inductors  $L_1$ ,  $L_2$ ,  $L_3$  and the capacities  $C_1$ ,  $C_2$ ,  $C_3$  form input filters and are meant to approximate the absorption of the sinusoidal current from the sources  $v_R$ ,  $v_S$  and  $v_T$ .

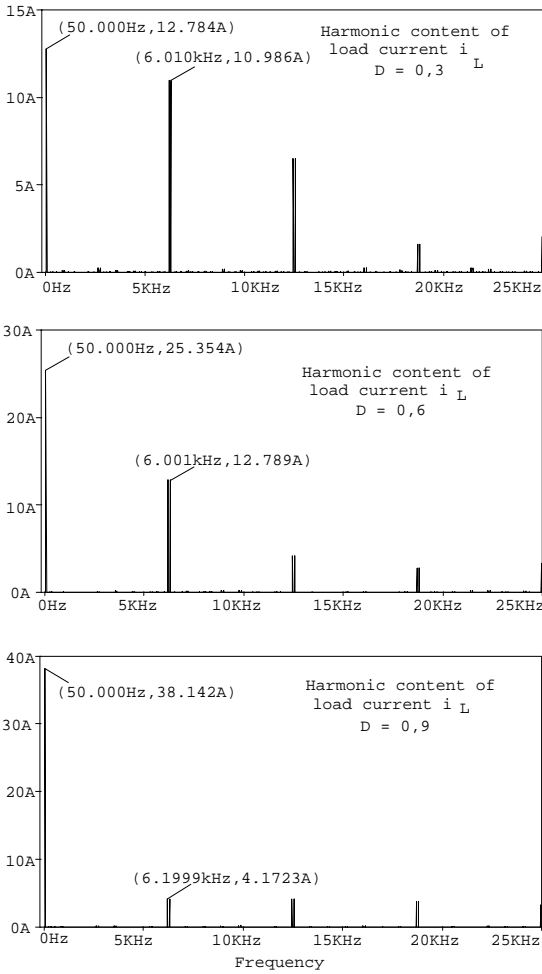


Figure 6. Harmonic contents of load current  $i_L$ .

### Simulation results

The presented power circuits of the three-phase ac choppers were tested by simulation. A strong inductive load was considered with  $R_L = 7$  ohms,  $L_L = 32$  mH, and amplitude of mains phase voltage  $V\sqrt{2} = 310V$ . Carrier frequency was  $f_s = 1/T_s = 6$  kHz and  $m = f_s/f = 120$ . Figure 4 shows the waveforms of the source current  $i_R$  for three values of the duty factor  $D$ .

Figure 5 presents the waveforms of the voltage  $v_{SR}$  and of the current  $i_L$  for  $D = 0,9$ .

Figure 6 shows the harmonic contents of the load current  $i_L$  for three values of the duty factor  $D$ .

Figure 7 shows the harmonic contents of the load voltage  $v_L$  for three values of the duty factor  $D$ .

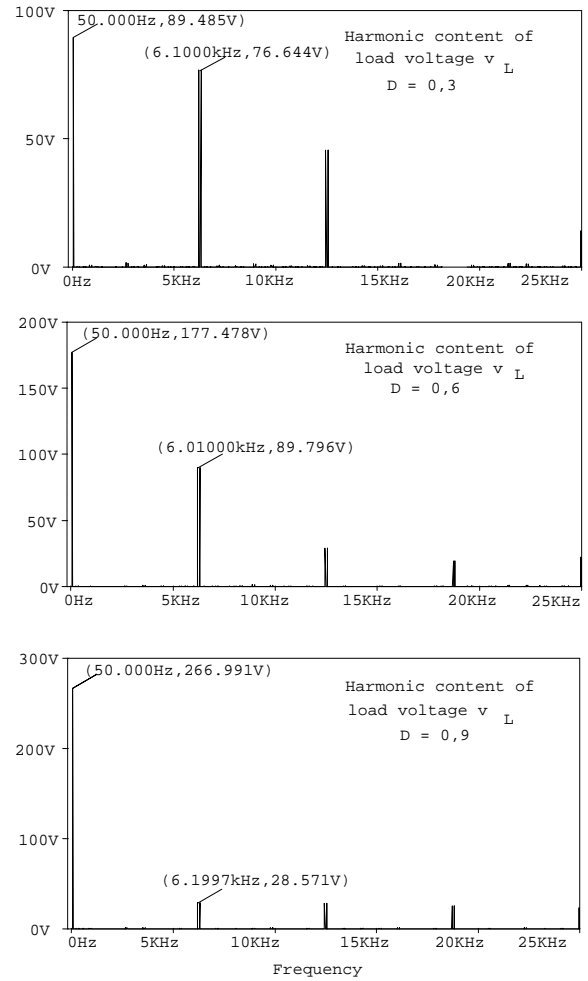


Figure 7. Harmonic contents of load voltage  $v_L$ .

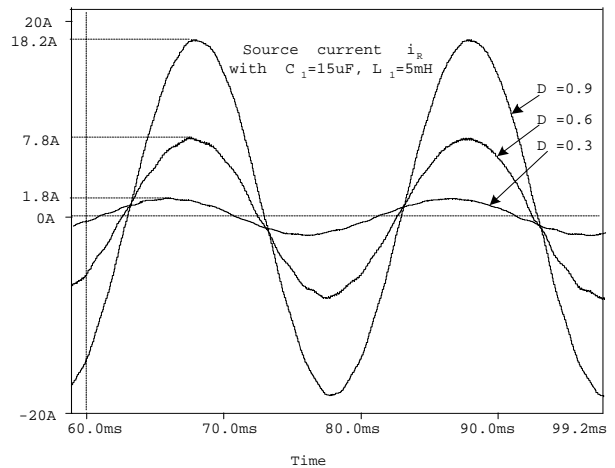


Figure 8. Source current  $i_R$  waveforms.

In order to approximate the sinusoidal currents absorbed  $i_R, i_S, i_T$ , we have consider that  $L_1 = L_2 = L_3 = 2mH$ , and the capacities  $C_1 = C_2 = C_3 = 16\mu F$ .

Figure 10 represent the waveforms obtained by

simulation of the absorbed currents  $i_R, i_S, i_T$ , sum of these currents  $i_R + i_S + i_T$ , and sum of the voltages  $v_R + v_S + v_T$ . Obtained results confirm theoretical affirmation presented in relation (2).

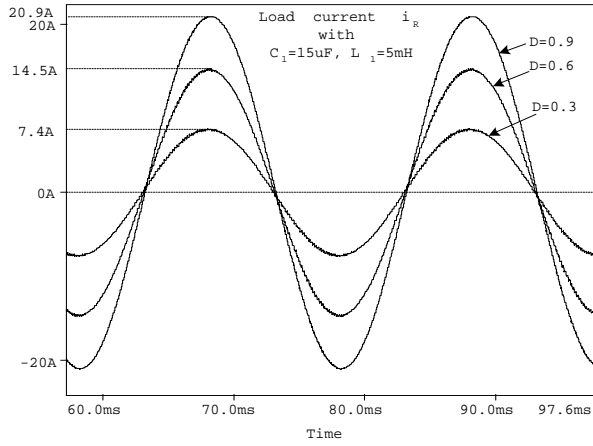


Figure 9. Load current  $i_L$

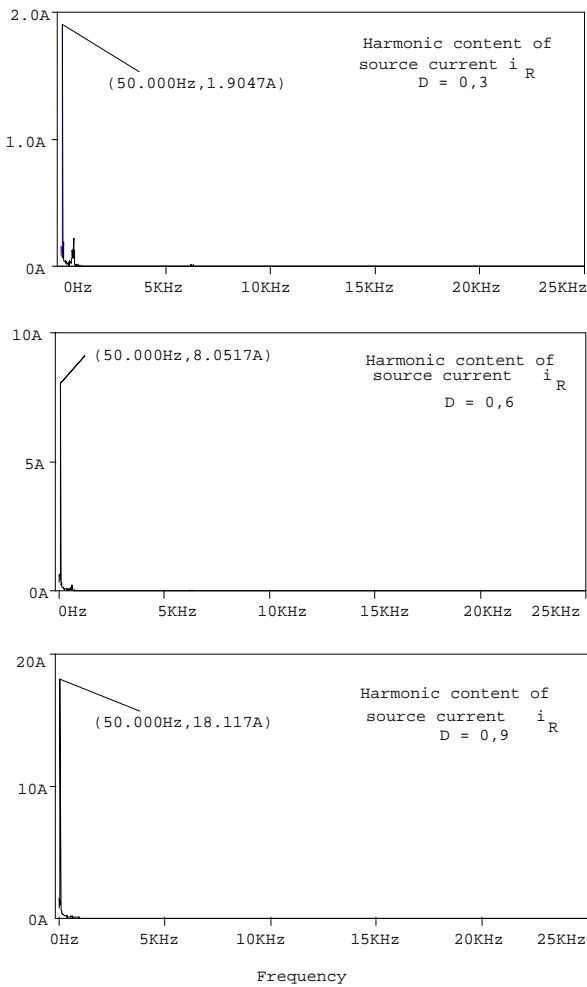


Figure 11. Harmonic contents of source current  $i_R$

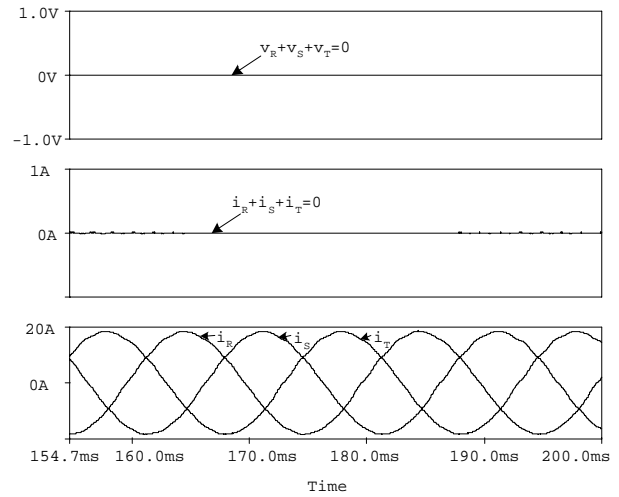


Figure 10. Source currents  $i_R, i_S, i_T$  waveforms, sum of the currents  $i_R + i_S + i_T$  and sum of the voltages  $v_R + v_S + v_T$

Figure 11 shows the harmonic contents of the

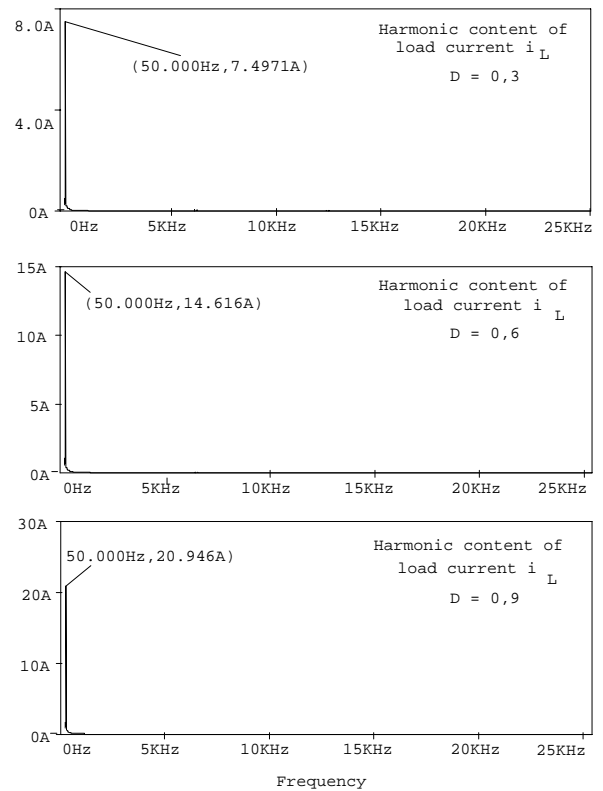


Figure 12. Harmonic contents of the load current source current  $i_R$ , Figure 12 presents the harmonic contents of the load current  $i_L$  and Figure 13 presents the harmonic contents of the load voltage  $v_L$  for three value of duty factor  $D$ . Figure 8 shows the input currents  $i_R$  and figure 9 presents the wave forms of the load current  $i_L$  for three value of duty factor  $D$ , when the

power circuit in Figure 3 is used, with  $C_1 = C_2 = C_3 = 15\mu\text{F}$ ,  $L_1 = L_2 = L_3 = 5\text{mH}$ ,  $C'_1 = C'_2 = C'_3 = 1\mu\text{F}$ . Sinusoidal waveforms for  $i_s$  have been obtained.

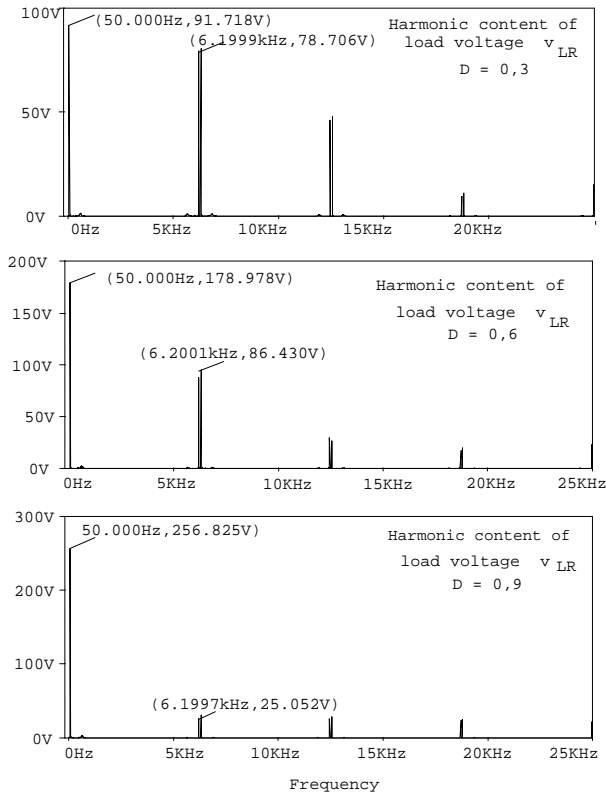


Figure 13. Harmonic contents of the load voltage

Figure 14 represent the waveforms obtained by simulation of the load voltage  $v_{LR}$ ,  $v_{LS}$ ,  $v_{LT}$ , and the control signal  $V_{com1}$ ,  $V_{com2}$ .

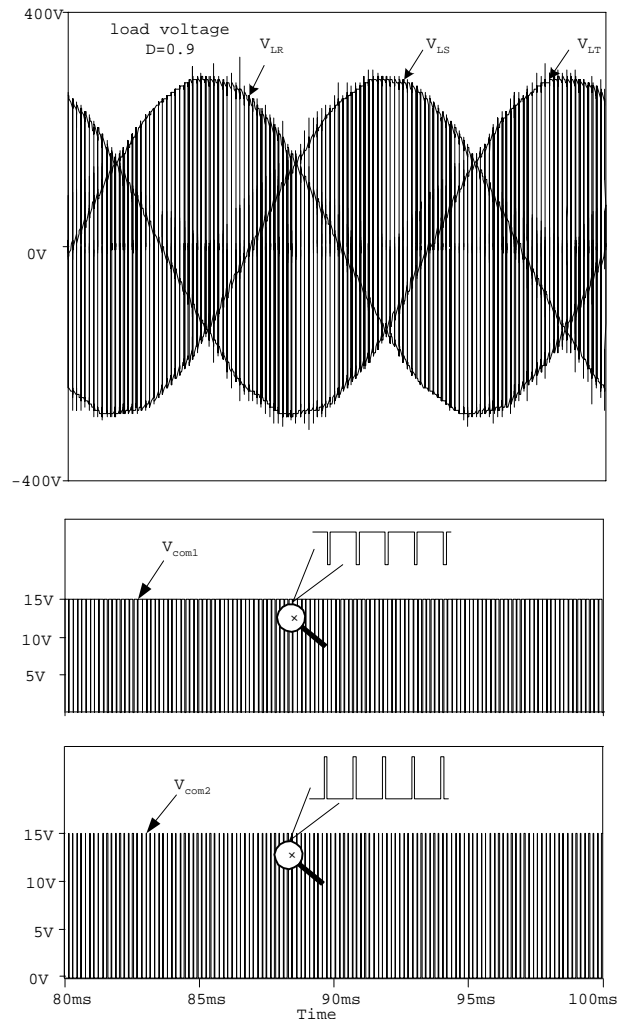


Figure 14. Load voltage  $v_{LR}$ ,  $v_{LS}$ ,  $v_{LT}$ , and the control signal  $V_{com1}$ ,  $V_{com2}$  for the duty factor  $D=0.9$

### Conclusion

The simulation results proved good performance of the three-phase ac chopper with IGBT's on high chopper frequency. A sinusoidal input current was obtained by using the power circuit with filter.

In the case of a symmetrical three-phase system, the ground wire is unusable. For this reason, the ground wire was not necessary in the power circuit.

### References

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